

## Visco-Elasticity

### 1 Standard linear solid

Consider the one-dimensional Standard-Linear-Solid (SLS) model, described in the left panel of the Fig. below. In this exercise we will explore its visco-elastic properties in much the same way that we did in class for the Maxwell and Kelvin-Voigt models.

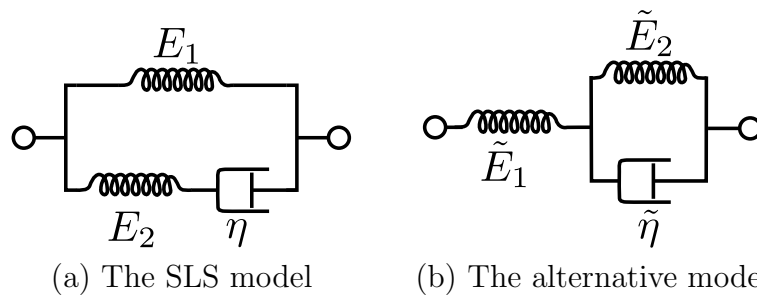


Figure 1:

- (i) Calculate  $G^{\text{SLS}}(t)$  and  $J^{\text{SLS}}(t)$ .
- (ii) Calculate  $G^*(\omega)$ . Find the effective Young's modulus for very short and very long time scales. Denote these quantities by  $E_0$  and  $E_\infty$ , respectively. Check that your finding agrees with the proper limits of the results of Q1(i). (writing  $J$  and  $G$  in terms of  $E_0$  and  $E_\infty$  might prove to be more elegant than with  $E_1$  and  $E_2$ ).
- (iii) **QUALITATIVE QUESTION:** Plot the loss and storage moduli  $G'(\omega)$  and  $G''(\omega)$  on a logarithmic  $\omega$  scale for the case  $E_1 = E_2$ . If you were to transfer waves through an SLS material, which frequencies would be transmitted and which attenuated?
- (iv) Calculate  $\varepsilon(t)$  when the stress increases from 0 to  $\sigma_0$  over a time scale  $T$ . To make things concrete, take the stress to be

$$\sigma(t) = \begin{cases} 0 & t < 0 \\ \sigma_0 (1 - e^{-t/T}) & t > 0 \end{cases} .$$

For simplicity, also set  $E_1 = E_2$ . Plot  $\varepsilon(t)$  for the cases that  $T$  is (i) much larger than, (ii) much smaller than, and (iii) roughly equal to the relevant internal time-scale of the system (for the two extreme cases you should know the answer without any further algebra!).

- (v) Consider an alternative model, defined in Fig. 1(b). Show that it is exactly equivalent to the SLS model, but with renormalized visco-elastic constants. That is, show that one can choose  $\tilde{E}_1, \tilde{E}_2, \tilde{\eta}$  so that this model will have the same rheological properties as the SLS model with

parameters  $E_1, E_2, \eta$ .

- (vi) **QUALITATIVE QUESTION:** The name “SLS” model suggests that it describes a solid. What is the basic property of solids that the SLS model possess but that Maxwell model doesn’t? And what is the problem with Kelvin-Voigt model?

## 2 Creep compliance and stress relaxation moduli

Prove the general identity

$$\int_0^t G(t-t')J(t')dt' = t , \quad (1)$$

and verify it explicitly for the KV and M models. Hint: Laplace transform.

## 3 Stored elastic energy

Define  $W_{sto}$  as the elastic energy stored in a quarter of an oscillatory cycle. Recall the definition of the phase  $\delta$  (Eqs. (9.39)-(9.40) in Eran’s lecture notes) and show that

$$\frac{W_{dis}}{W_{sto}} \sim \tan \delta . \quad (2)$$

## 4 Distribution of relaxation times

For some systems which exhibit a wide distribution of relaxation times the stress relaxation modulus can be written as a weighted sum of exponential decays with different decay rates:

$$G(t) = \int_{\tau} f(\tau)e^{-\frac{t}{\tau}}d\tau , \quad (3)$$

where  $f(\tau)$  is the relaxation times distribution function. If the relaxation times depend on some energy barrier  $\Delta$ , this can be written as

$$G(t) = G_0 \int_{\Delta} P(\Delta)e^{-\frac{t}{\tau(\Delta)}}d\Delta , \quad (4)$$

where  $P$  is the energy barrier distribution function. When the transitions are thermally-activated and the energy barriers are much larger than the thermal energy scale ( $\Delta \gg k_B T$ ) the rate of escape times varies exponentially with the barrier height:

$$\tau(\Delta) \simeq \tau_0 e^{\frac{\Delta}{k_B T}} . \quad (5)$$

This is a fundamental result, derived by Arrhenius (1889, for chemical reactions) Eyring (1935) and Kramers (1940, for Brownian motion under an external potential) and the factor  $e^{\frac{\Delta}{k_B T}}$  is usually termed “Arrhenius factor” or “rate factor”.

- (i) Assume that  $\Delta$  is uniformly distributed between  $\Delta_{min}$  and  $\Delta_{max}$ , and calculate  $G(t)$ . Express your answer using rate variable  $\nu(\Delta) \equiv 1/\tau(\Delta)$ . You might find that the exponential integral function,  $E_1(x) \equiv \int_1^\infty \frac{e^{-xy}}{y} dy$ , is useful.
- (ii) Choose  $\nu_{min} \equiv \nu(\Delta_{min})$  and  $\nu_{max} \equiv \nu(\Delta_{max})$  to be well separated and plot  $G(t)$ . What is special about this result? How does it differ from standard relaxation?
- (iii) Obtain an analytic expression (you are allowed to be wrong by an additive constant) for  $G(t)$  for an intermediate asymptotic regime,  $\nu_{min}^{-1} \ll t \ll \nu_{max}^{-1}$ . This is a simple mathematical model for slow/glassy relaxation emerging from a broad distribution of relaxation times (activation barriers in this case).

For the interested, such a model has been proposed already by [Primak, Phys. Rev. \*\*100\*\*, 1677 \(1955\)](#), and later on by [Kimmel and Uhlmann, J. Appl. Phys. \*\*40\*\*, 4254 \(1969\)](#). This model has been revisited by Ariel Amir, Yuval Oreg and Joe Imry from the institute. See for example [Amir, Oreg and Imry, PNAS \*\*109\*\*, 1850–1855 \(2012\)](#).